

# **The Role of Degradation on Foaming of Various Amine Solvents in Model Columns**

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## Overview

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Foam: the problem in amine based post-combustion carbon capture

- Background on foam formation

Experimental methodology and modification to ASTM standard

Initial investigations on oxidative degradation (MEA, MDEA, AEP, AMP)

- Assessing the interaction of input variables on the foaming of both 'clean' and degraded solvents

Further investigations on thermal degradation (MEA, MDEA, AEP, AMP)

- Relating the changes in physical properties due to degradation on the resulting foaming of degraded solvents

Conclusions

## Problem of Foaming

- Foaming is one of the **main operational problems** for alkanolamine based processes: Natural Gas Sweetening  
Post-Combustion Carbon Capture
- **Consequence: Loss of liquid → ↓ of CO<sub>2</sub> absorption capacity**
  - directly by: change in volume
  - indirectly by: change in solution composition  
reduction in mass transfer area
  - Financial losses
- Believed to be caused by contamination
- Ameliorated using anti-foam agents and other reactive efforts

## Foam Quantification

1. Bikerman model: Foamingness =  $\Sigma = \frac{H_o}{j}$  ← Foam height  
← Superficial gas velocity

This model is said not to depend on:

- Experimental apparatus (cell size and dimensions, frit porosity, etc...)
- Gas pressure
- Solution volume (i.f.f. volume is sufficiently large)

Gas flow rate must be in a regime that is neither 'too slow' nor 'too fast'

## Foam Quantification

1. Bikerman model: Foaming(= )  $\Sigma = \frac{H_o}{j}$  ← Foam height  
← Superficial gas velocity

2. Buckingham – Pi derived model:  $\Sigma = k \frac{\mu_s}{\sqrt{\sigma_s \rho_s}}$  ← Viscosity (dynamic)  
← Density  
← Surface tension

This predictive model uses a proportionality constant, k, to accommodate variability in foaming liquids.

An subsequent attempt to include bubble radius has been made, but has not been generalized in any acceptable manner

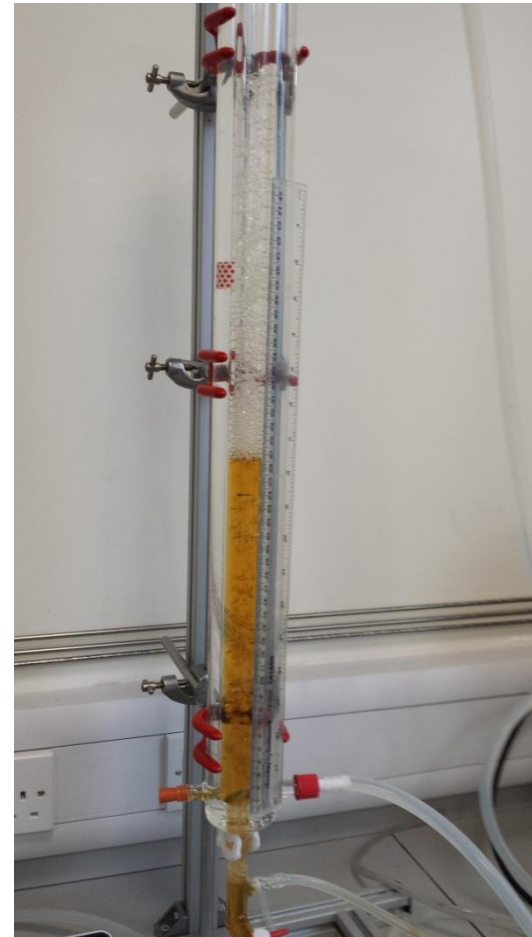
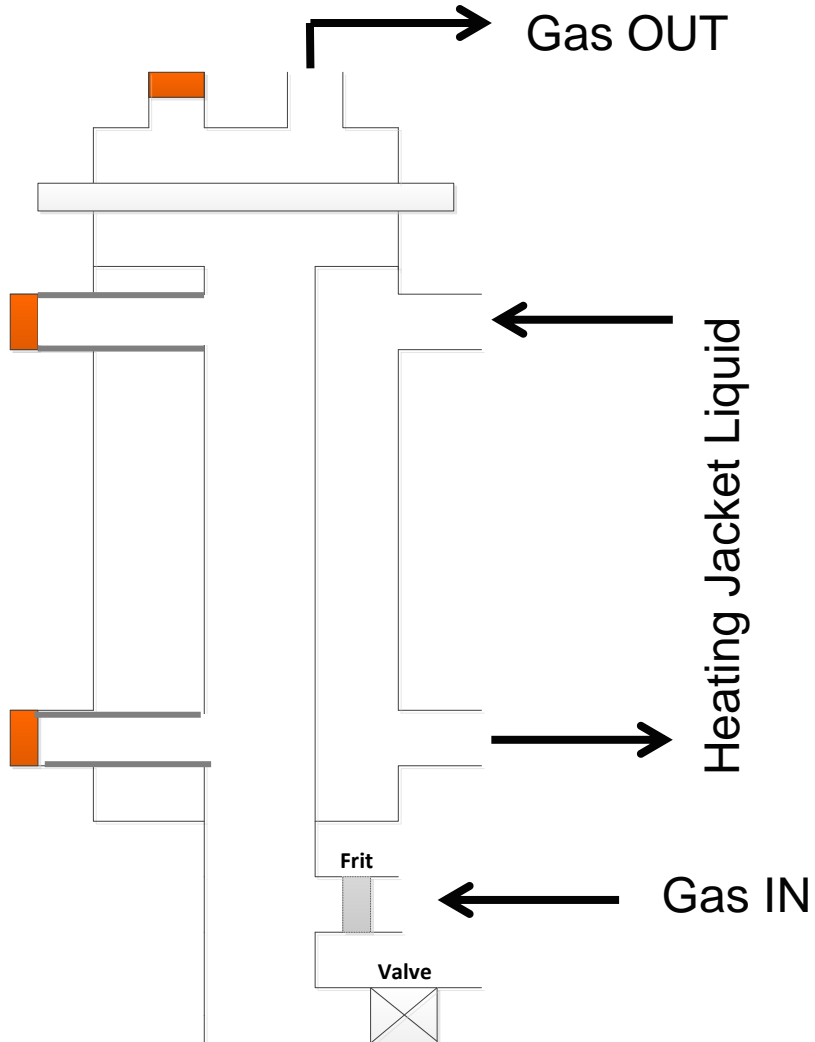
# Foam Quantification

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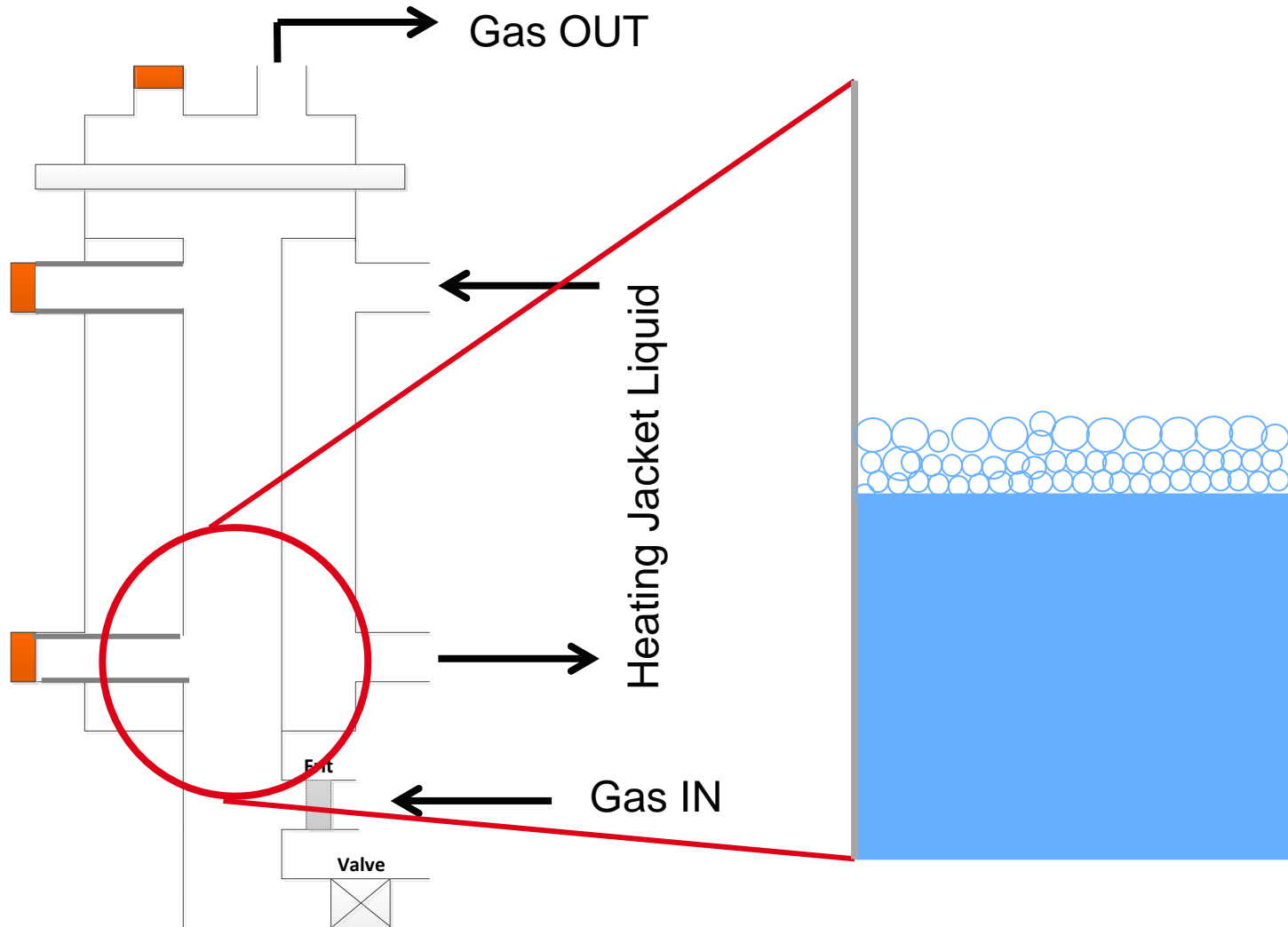
2. Buckingham – Pi derived model:  $\Sigma = k \frac{\mu_s}{\sqrt{\sigma_s \rho_s}}$  ← Viscosity (dynamic)  
 ← Density  
 ← Surface tension

3. Non-dimensional analysis:  $Ca \left( \frac{H_o}{r_o} \right) = k \left( \frac{Re}{Fr} \right)^n$  ←  $\frac{\text{Gravitational Forces}}{\text{Viscous Forces}}$   
 ↑  
 $\frac{\text{Viscous Forces}}{\text{Surface tension Forces}}$  ← Bubble radius

# Experimental Methodology

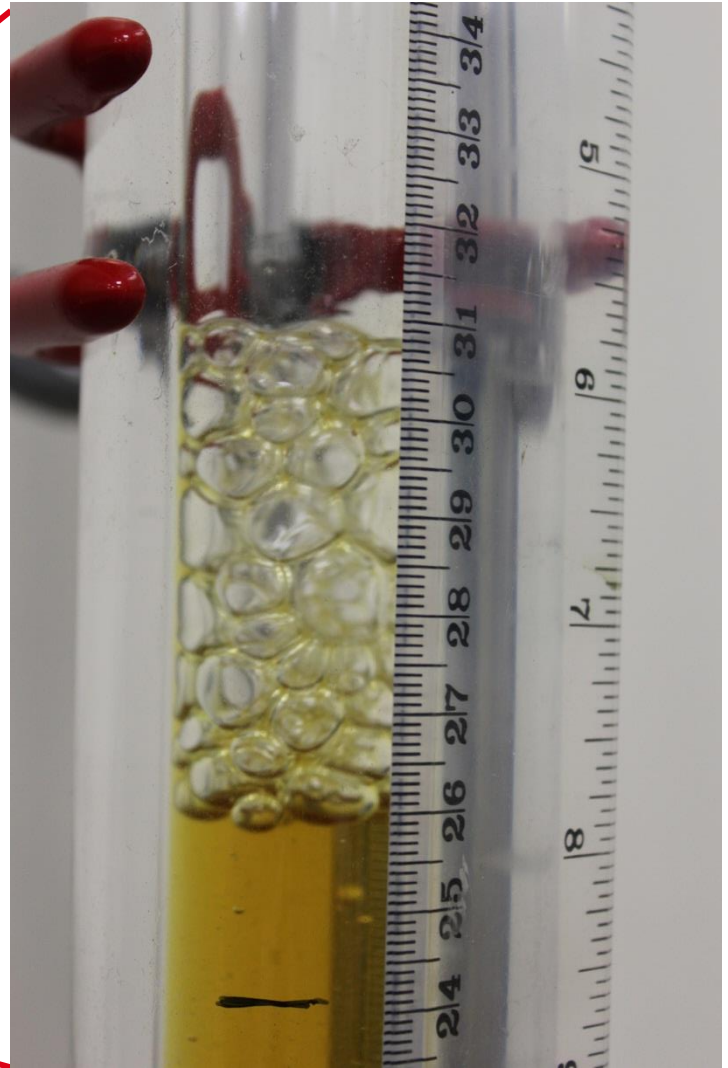
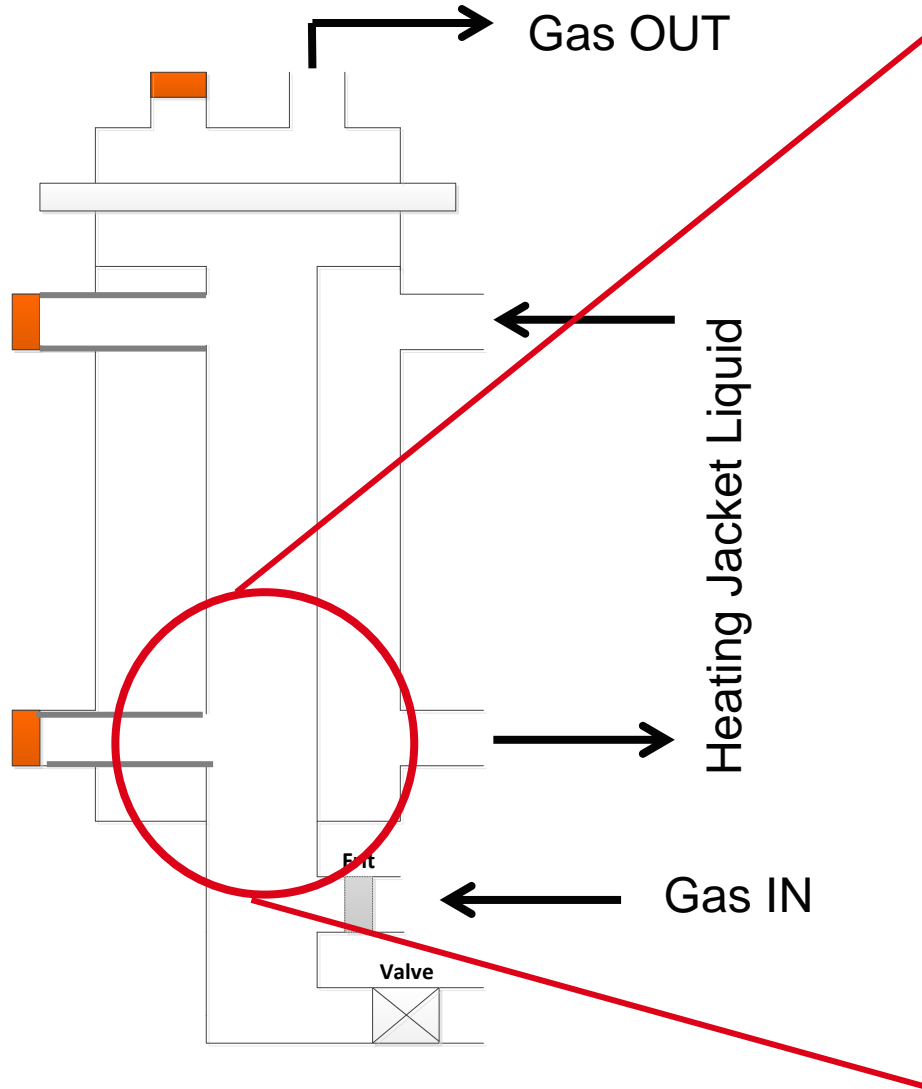


# Experimental Methodology

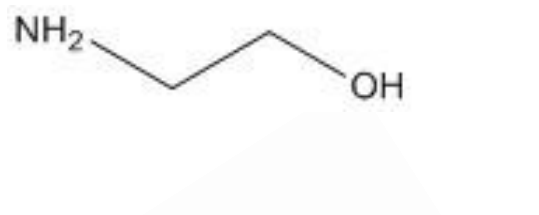
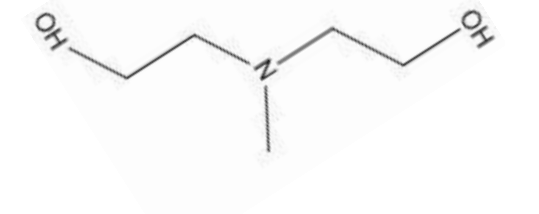
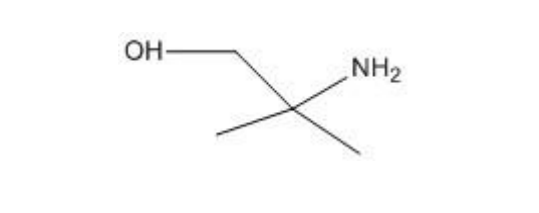
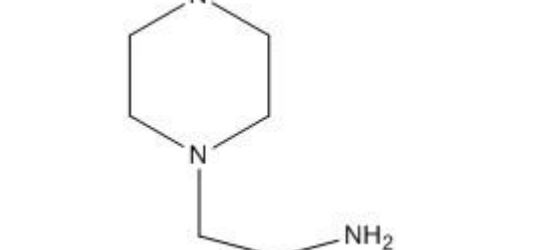




# Experimental Methodology

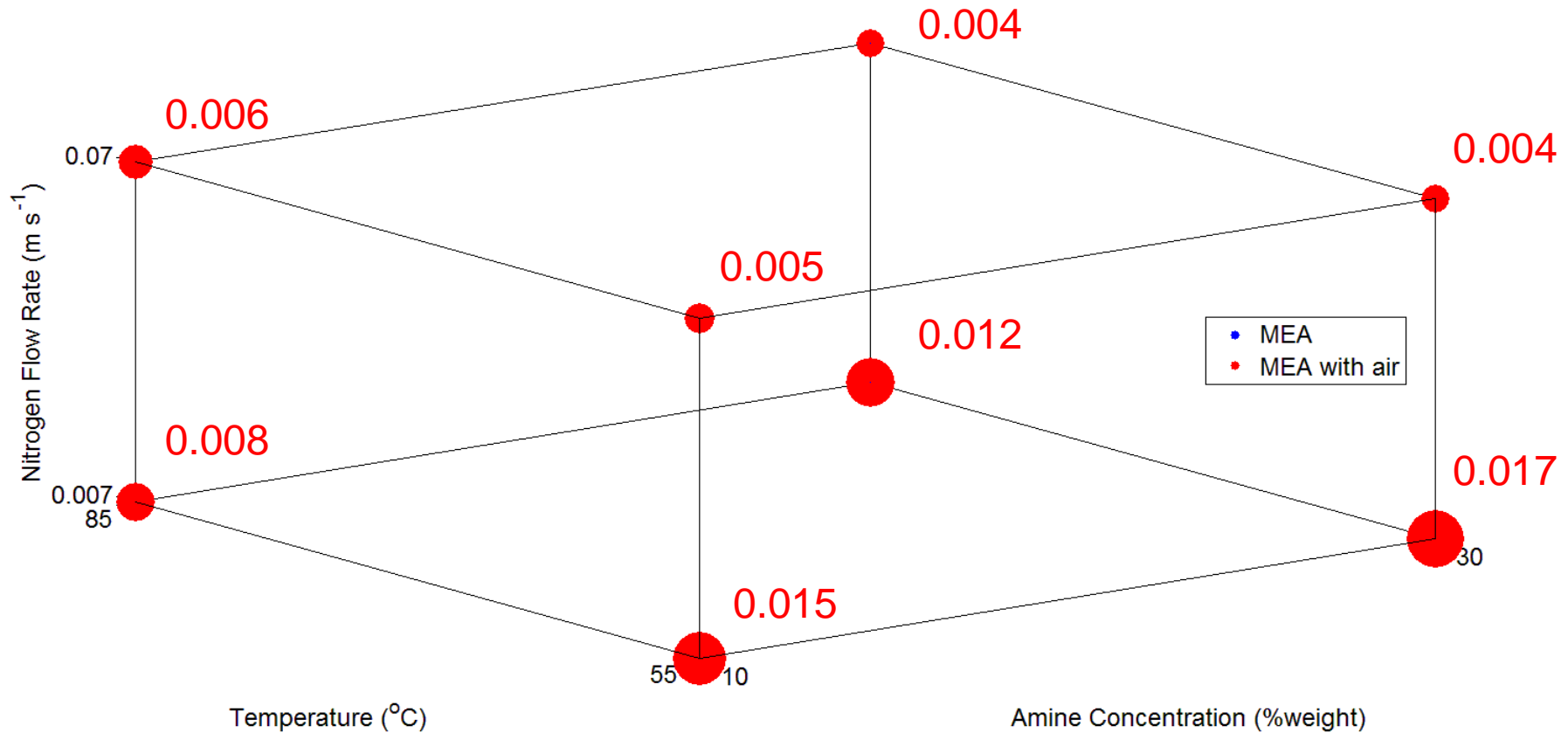


## Amine Solvents

<p>Monoethanolamine (MEA)</p>	 <chem>NCCCO</chem>	<p>#1: Primary</p>
<p>Methyldiethanolamine (MDEA)</p>	 <chem>CN(CCCO)CCO</chem>	<p>#1: Tertiary</p>
<p>2-amino-2-methylpropanol (AMP)</p>	 <chem>CC(C)(O)N</chem>	<p>#1: Primary</p>
<p>1-(2-aminoethyl)-piperazine (AEP)</p>	 <chem>NCCN1CCNCC1</chem>	<p>#1: Primary #2: Secondary #3 Tertiary</p>

# **INITIAL INVESTIGATIONS (OXIDATIVE DEGRADATION)**

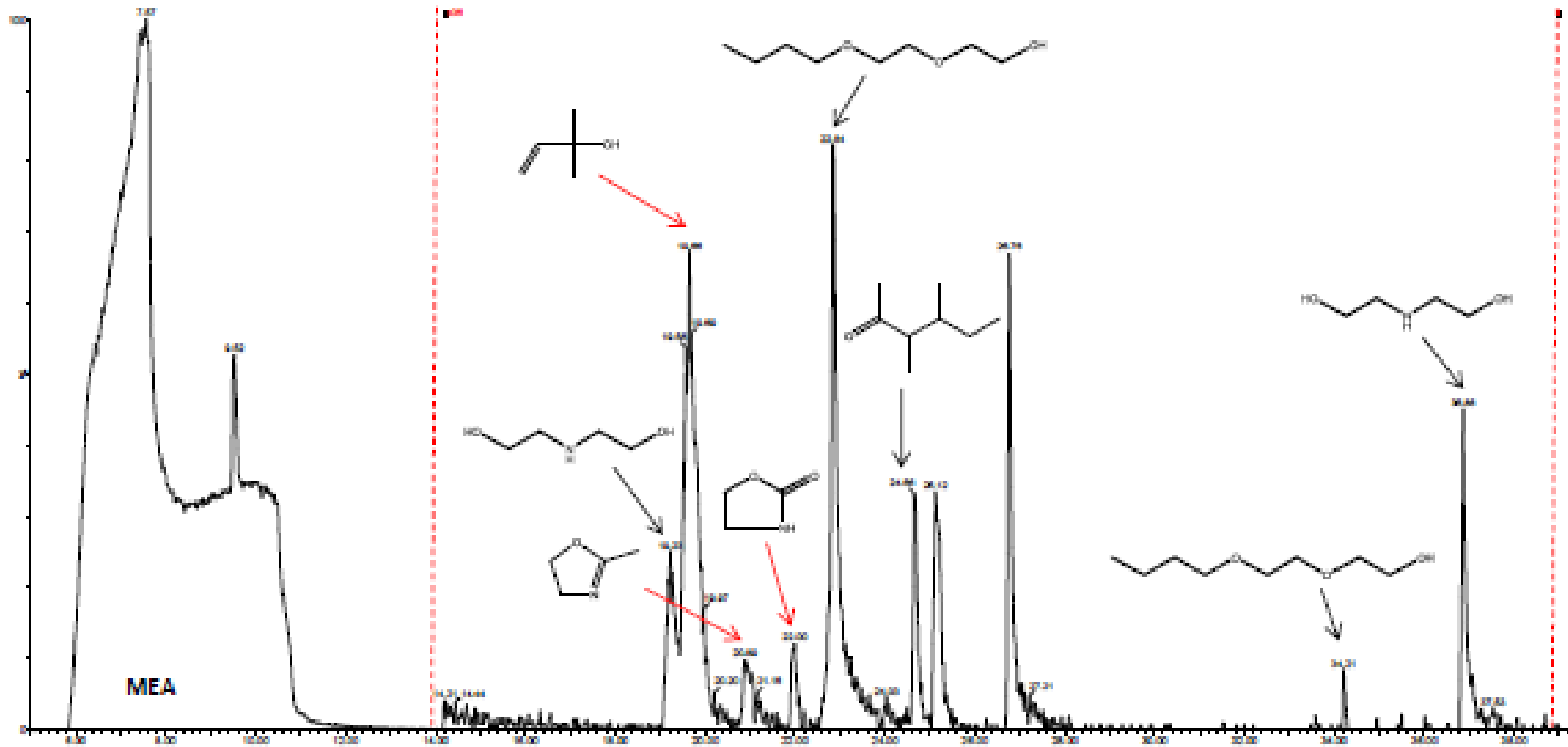
# MEA Foaminess



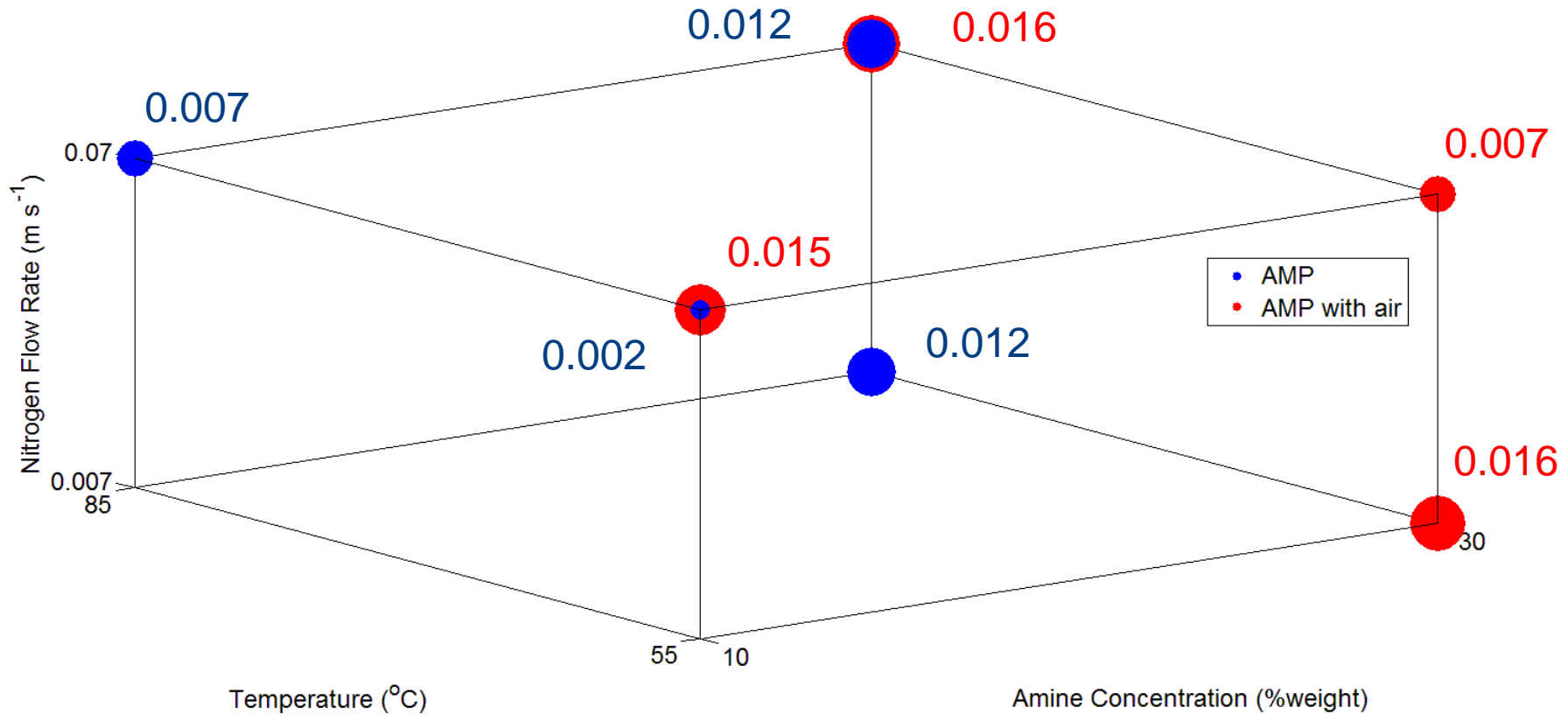
'Clean' MEA : No Foaminess

Oxidized MEA: Low Nitrogen Flow Rate → ↑ Foaminess

# MEA Oxidative Degradation



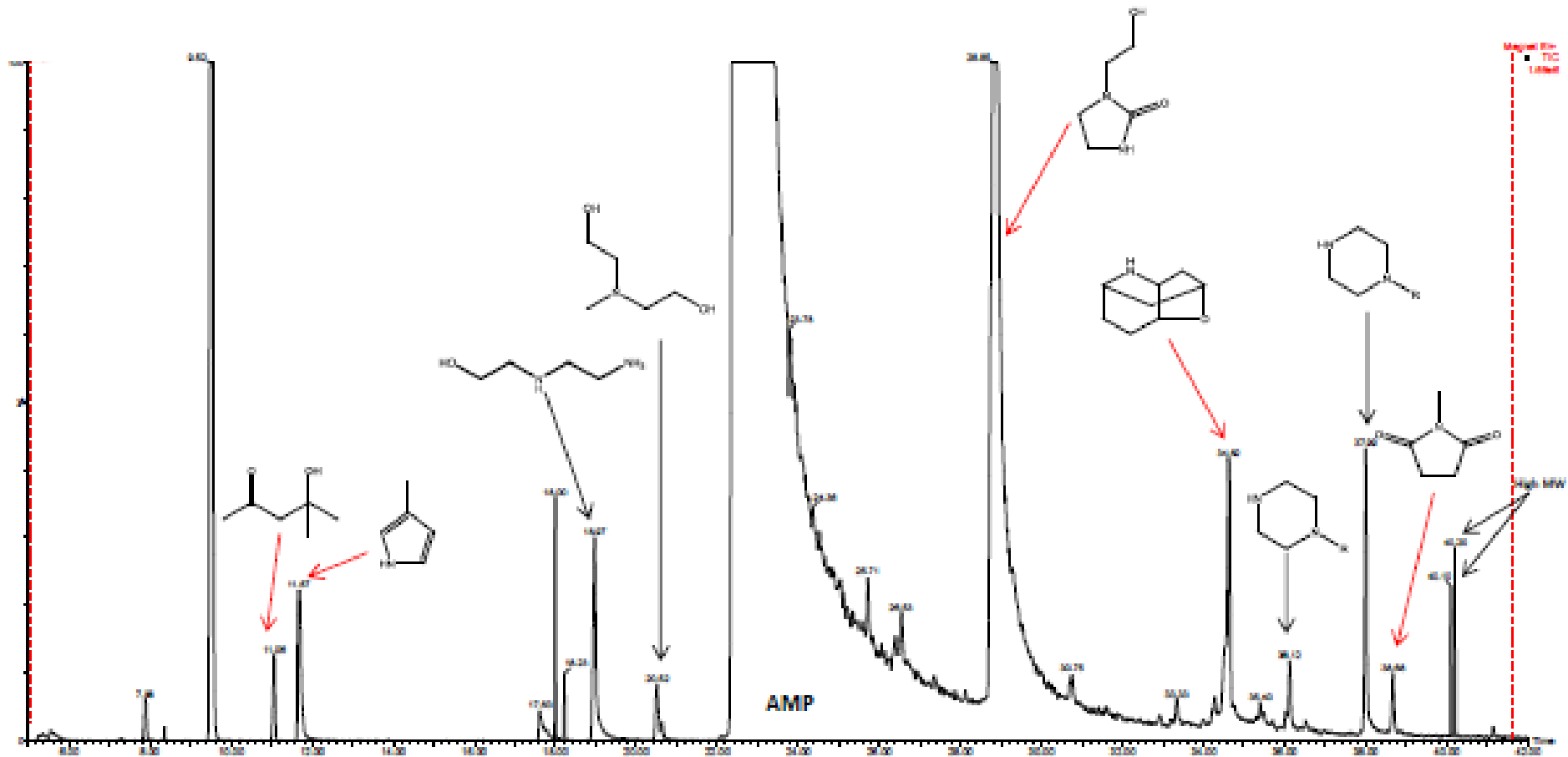
# AMP Foaminess



'Clean' AMP: High Temperature → Foaminess

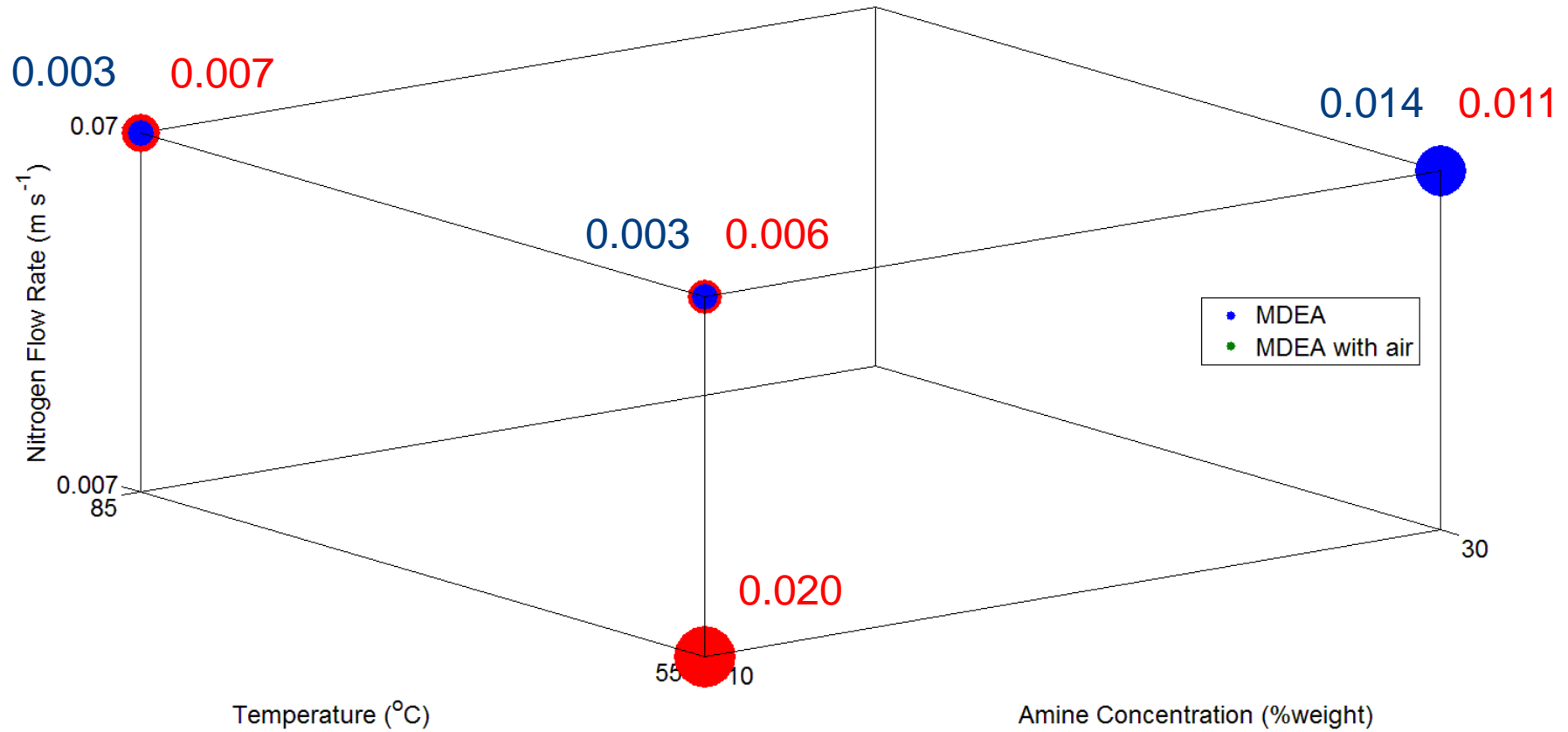
Oxidized AMP: Low Temperature → Foaminess

# AMP Oxidative Degradation



Significant degradation products

# MDEA Foaminess

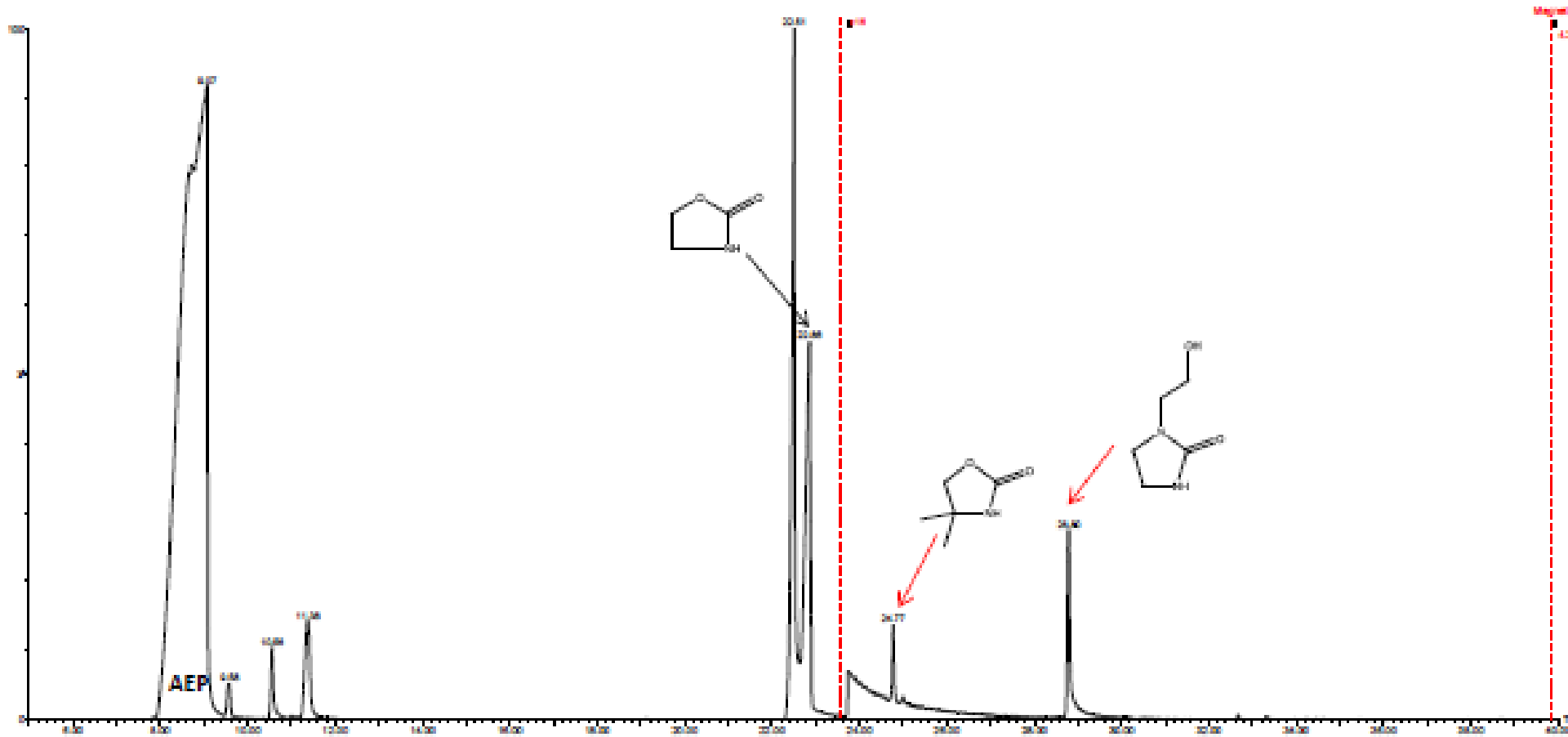


'Clean' MDEA : High Nitrogen Flow Rate → Foaminess

Oxidized MDEA ~ 'Clean' MDEA



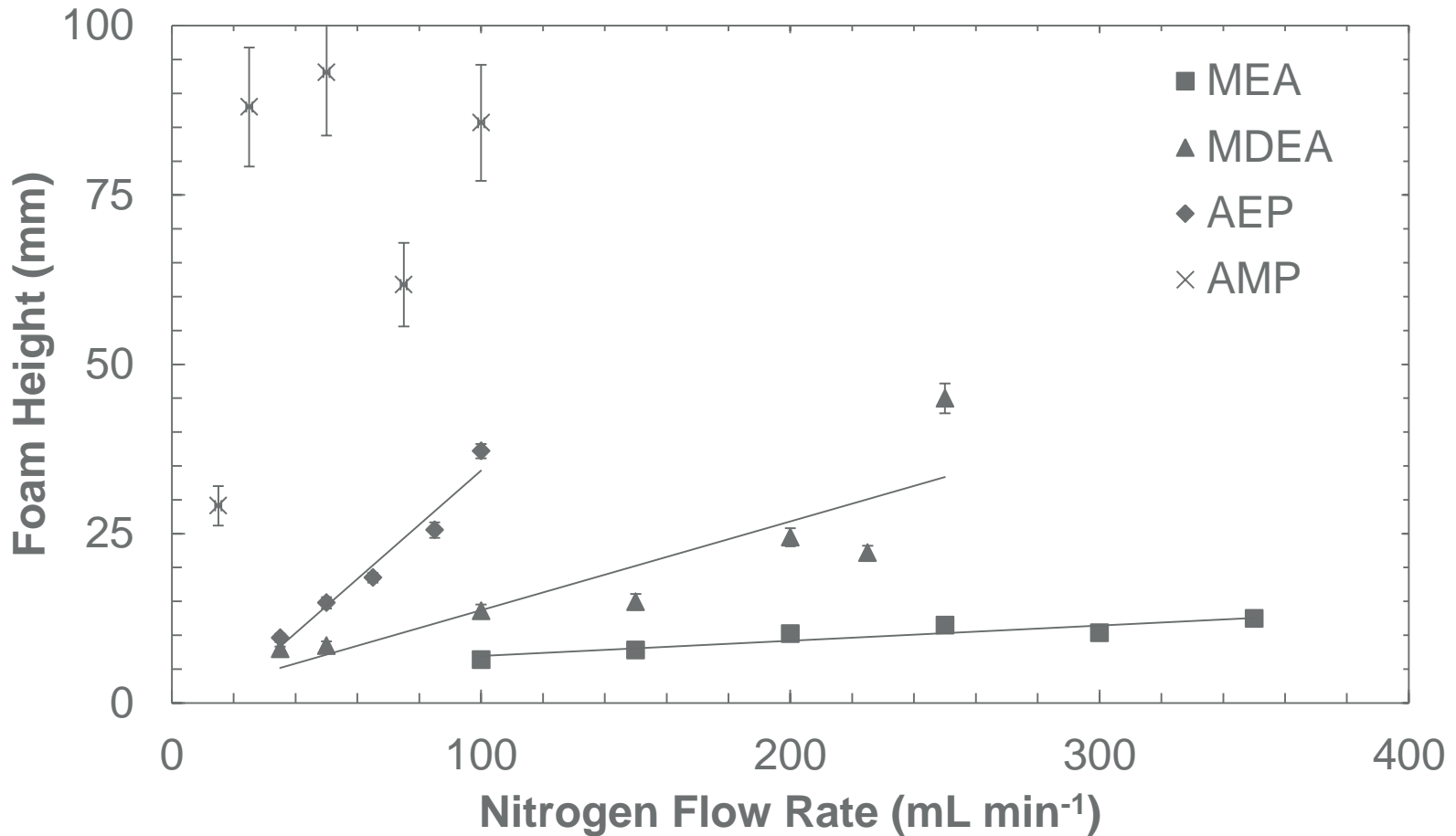
# AEP Oxidative Degradation



Nominal degradation products

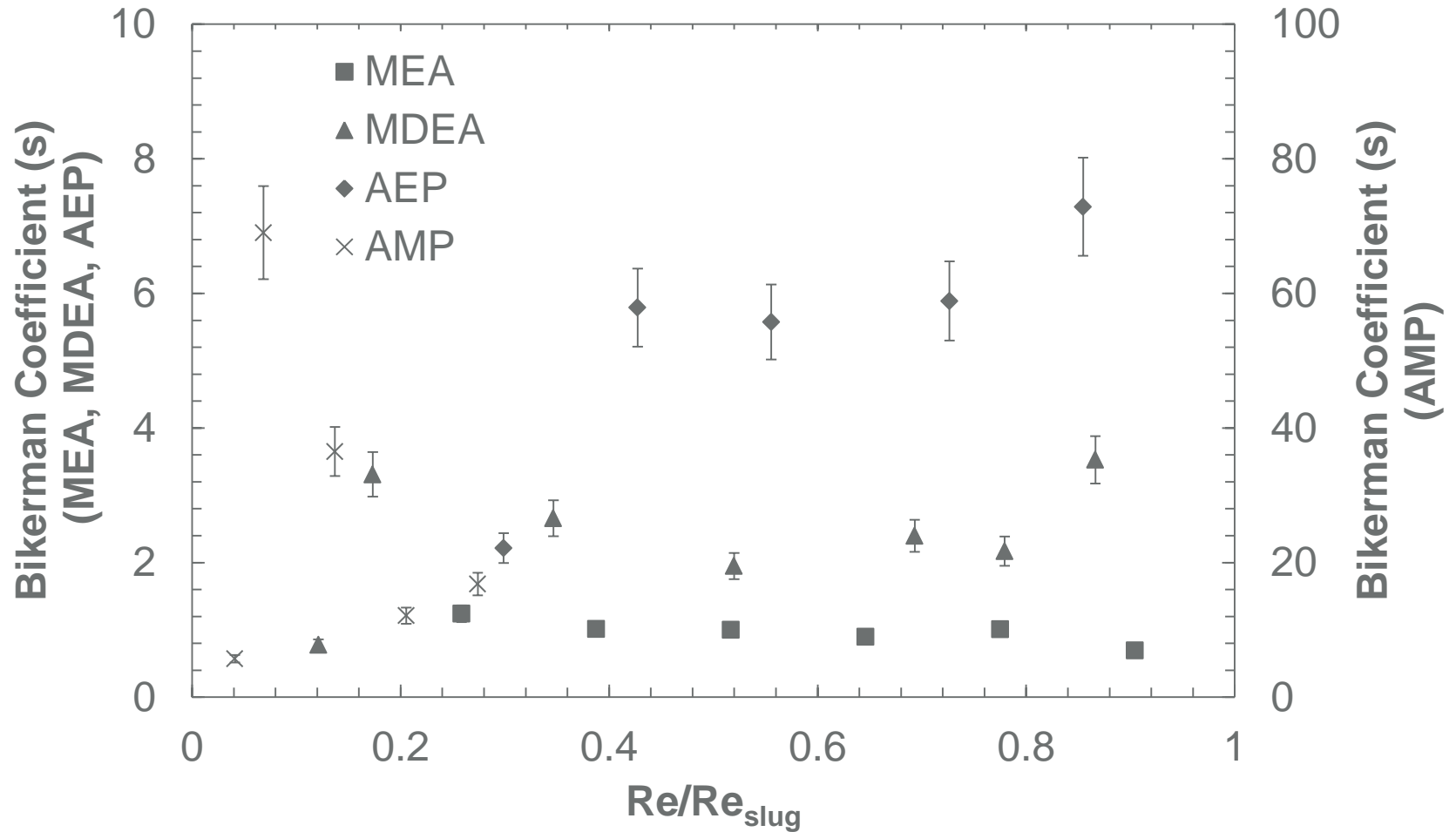
# **FURTHER INVESTIGATIONS (THERMAL DEGRADATION)**

## Amine Solvent Foaming – Bikerman Model



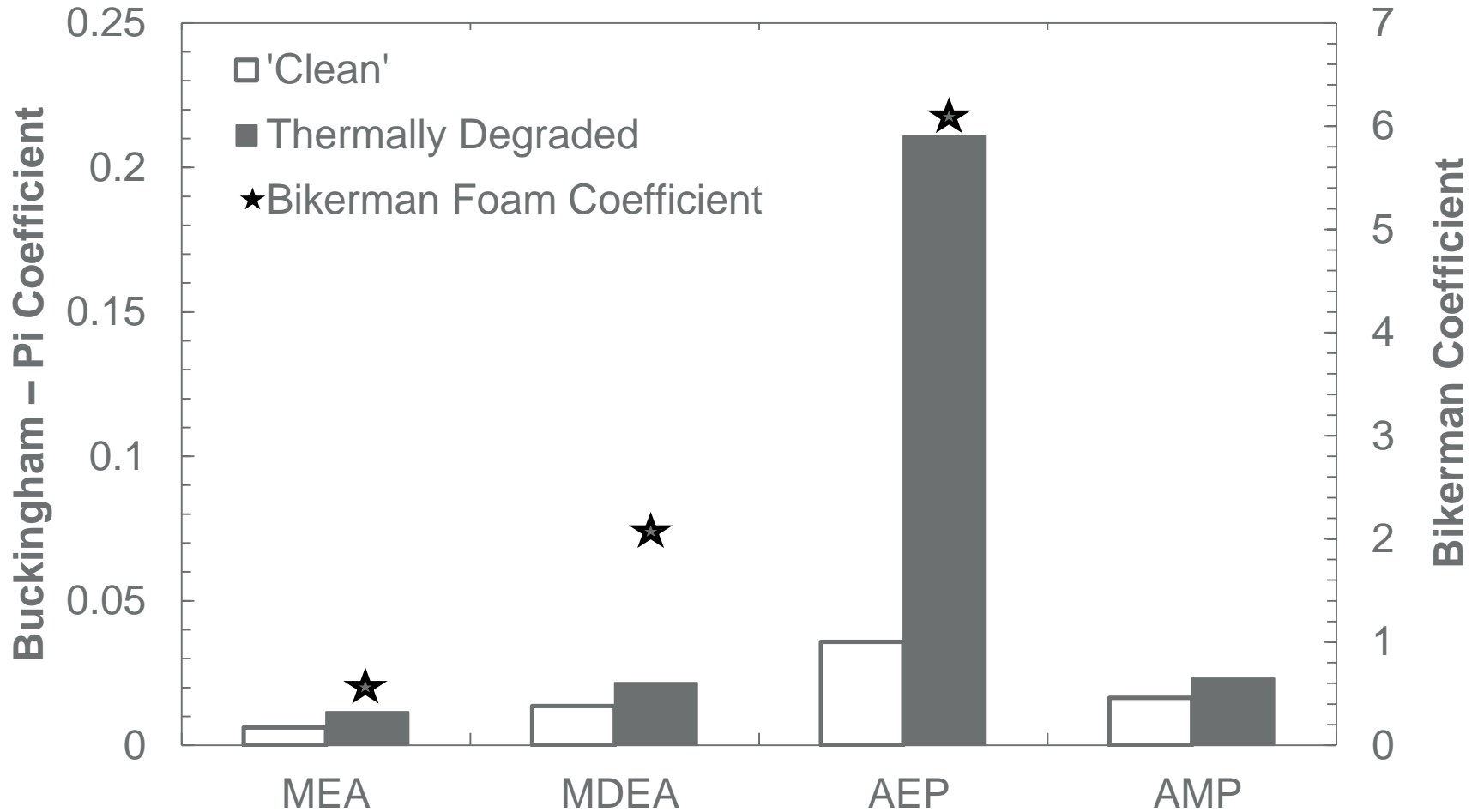
MEA, MDEA, AEP all demonstrate likely linear relationships,  
(as suggested by the Bikerman model)

## Amine Solvent Foaming – Improving Bikerman Model

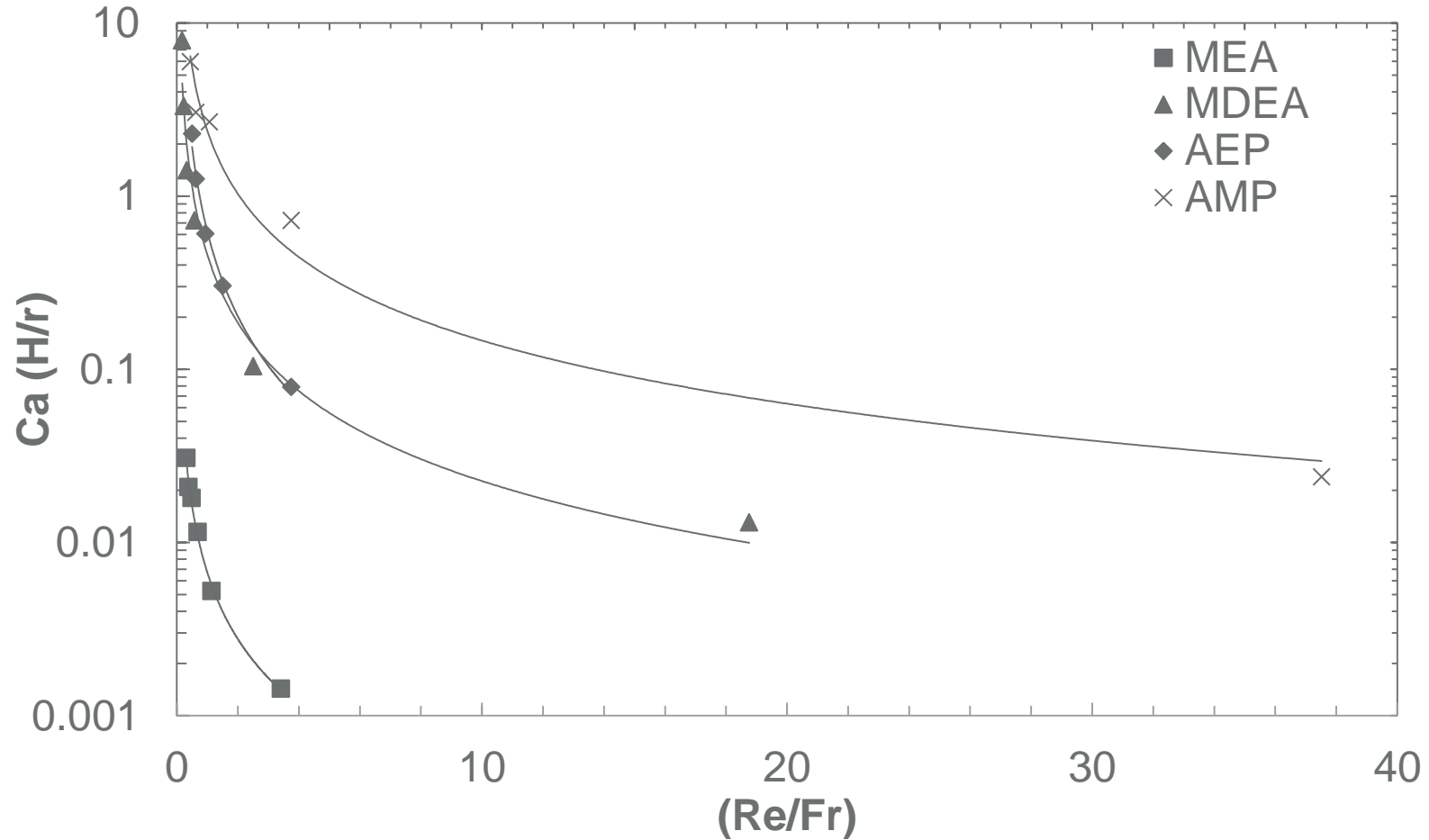


MEA, MDEA, AEP now scale approximately to a constant across full foaming to slugging regime

## Amine Solvent Foaming – Buckingham – Pi Model

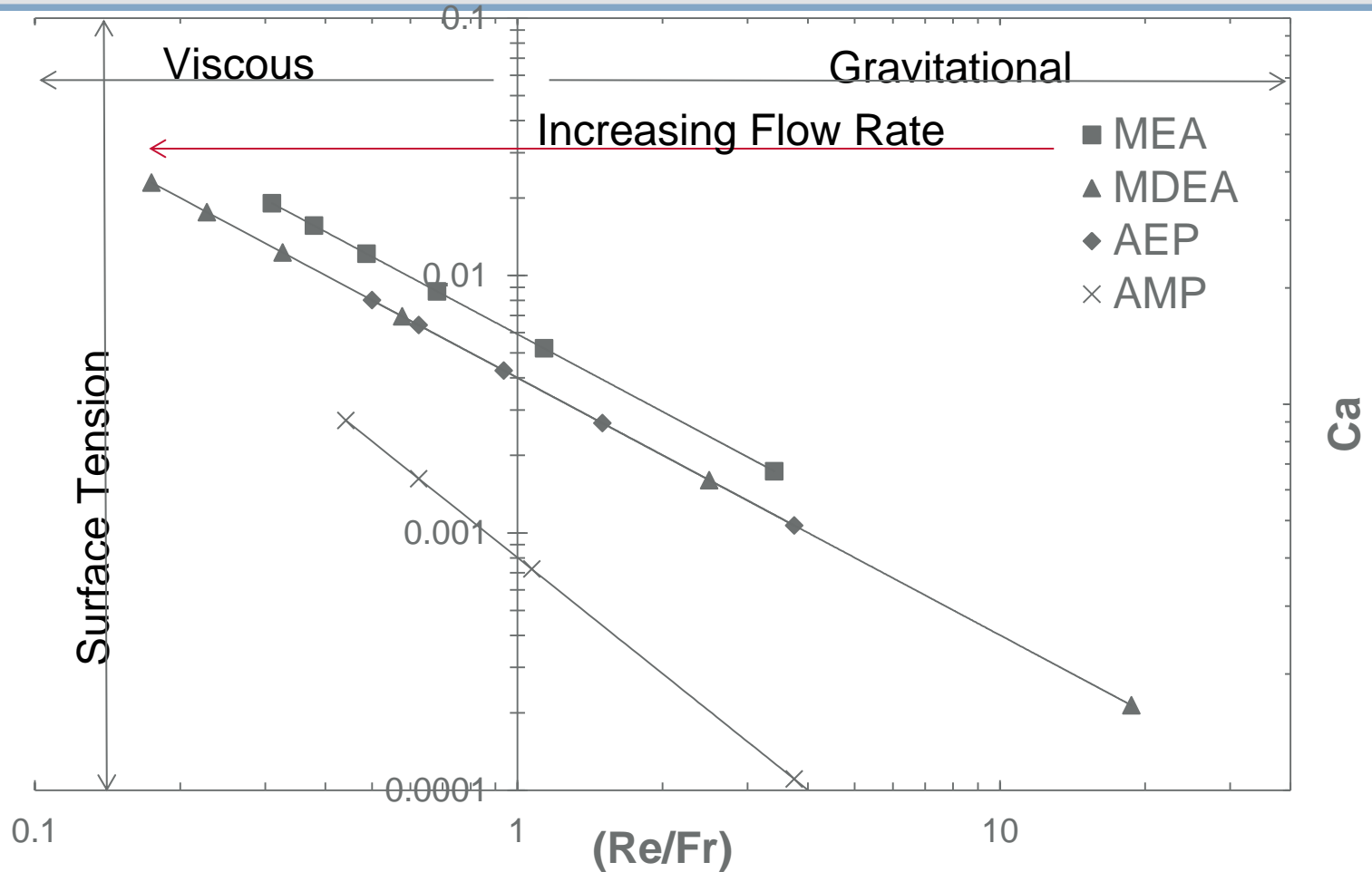


# Amine Solvent Foaming – Non-Dimensional Analysis



Power law fitting indicates that the power  $\sim -1.4$  for all four amine solvents  
Pre-exponential factor varies by three order of magnitude

# Amine Solvent Foaming – Non-Dimensional Analysis



Surface tension dominates strongly

Viscous forces play a role at high flow rates, gravitational at low ones

## Conclusions

The foaming behavior of amine solvents are NOT consistent and must be considered individually before forming classifications

'Clean' MEA and AEP do not foam ; MDEA and AMP do foam

The formation of degradation products → changes solvent physical properties → changes foaming behavior

- Oxidative < Thermal Degradation induced foaming

Unstable foam: MEA, MDEA, AEP ; Stable foam: AMP

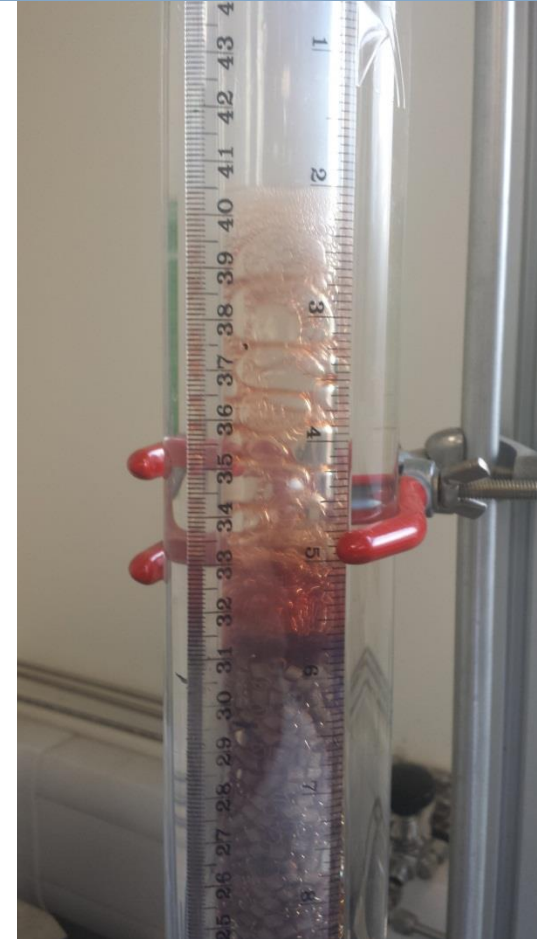
Non-dimensional method appears the best but still provides limited physical understanding of the data collected



## Acknowledgements

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